

Find the appropriate stoichiometric coeffs for the following chemical reactions by conserving the number of atoms of each element between the reactants and products.



$$\text{Fe balance} \rightarrow a_3 - a_1 = 0$$

$$\text{O balance} \rightarrow a_3 + 2a_4 - 2a_2 = 0$$

$$\text{S balance} \rightarrow a_4 - a_1 = 0$$

and $a_1 = \alpha \leftarrow$ chosen to give integer coeffs

In matrix form, these become

$$\begin{bmatrix} -1 & 0 & 1 & 0 \\ 0 & -2 & 1 & 2 \\ -1 & 0 & 0 & 1 \\ 1 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} a_1 \\ a_2 \\ a_3 \\ a_4 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ \alpha \end{bmatrix}$$

↑ program this into matlab (see reaction_eqns1.m) to get

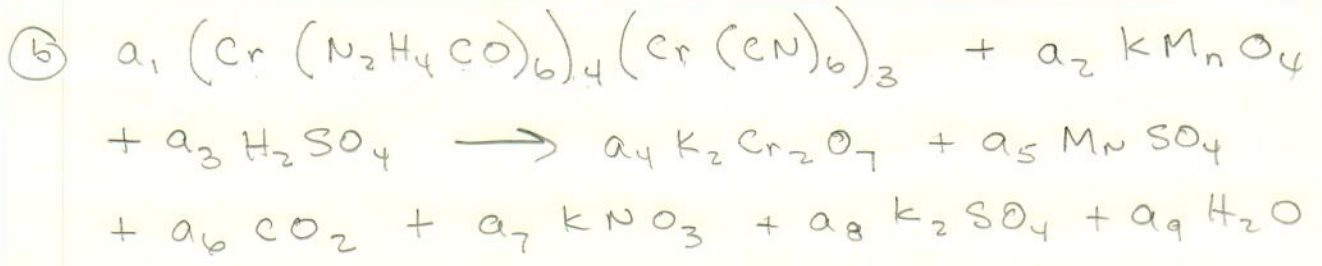
$$\text{with } \alpha > 1 \quad a_1 = 1 \quad a_2 = 1.5 \quad a_3 = 1 \quad a_4 = 1$$

\therefore let $\alpha = 2$ then

$$a_1 = 2 \quad a_2 = 3 \quad a_3 = 2 \quad a_4 = 2$$



(b)



K balance $\rightarrow 2a_4 + a_7 + 2a_8 - a_2 = 0$

Cr balance $\rightarrow 2a_4 - 7a_1 = 0$

O balance $\rightarrow 7a_4 + 4a_5 + 2a_6 + 3a_7 + 4a_8 + a_9$
 $- 24a_1 - 4a_2 - 4a_3 = 0$

Mn balance $\rightarrow a_5 - a_2 = 0$

S balance $\rightarrow a_5 + a_8 - a_3 = 0$

C balance $\rightarrow a_6 - 42a_1 = 0$

N balance $\rightarrow a_7 - 66a_1 = 0$

H balance $\rightarrow 2a_9 - 96a_1 - 2a_3 = 0$

and $a_1 = x$ chosen to give integer results

In matrix form, these become

$$\begin{bmatrix} 0 & -1 & 0 & 2 & 0 & 0 & 1 & 2 & 0 \\ -7 & 0 & 0 & 2 & 0 & 0 & 0 & 0 & 0 \\ -24 & -4 & -4 & 7 & 4 & 2 & 3 & 4 & 1 \\ 0 & -1 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & -1 & 0 & 1 & 0 & 0 & 1 & 0 \\ -42 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ -66 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ -96 & 0 & -2 & 0 & 0 & 0 & 0 & 0 & 2 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} a_1 \\ a_2 \\ a_3 \\ a_4 \\ a_5 \\ a_6 \\ a_7 \\ a_8 \\ a_9 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ x \end{bmatrix}$$

program above matrix in Matlab to give
with $\alpha = 1$

$$a_1 = 1 \quad a_2 = 117.6 \quad a_3 = 139.9 \quad a_4 = 3.5 \quad a_5 = 117.6$$

$$a_6 = 42 \quad a_7 = 66 \quad a_8 = 22.3 \quad a_9 = 187.9$$

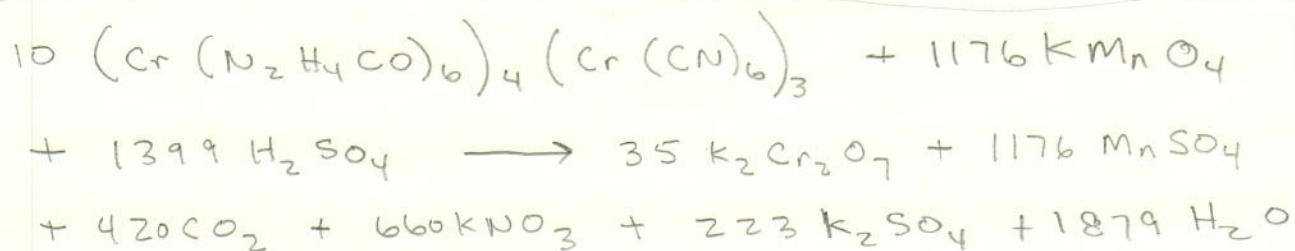
To make these integers, I need to multiply by 10
so set $\alpha = 10$

$$\text{then } a_1 = 10 \quad a_2 = 1176 \quad a_3 = 1399 \quad a_4 = 35$$

$$a_5 = 1176 \quad a_6 = 420 \quad a_7 = 660 \quad a_8 = 223$$

$$a_9 = 1879$$

thus, the balanced reaction eqn is:



```

%
% REACTION_EQNS1.M Balances for Chemical Reaction Equations
%
% This file computes the stoichiometric coefficients for a couple of reaction
% equations -- see the hand documentation for the development of the appropriate
% matrix equations...
%
% File prepared by J. R. White, UMass-Lowell (last update: Nov. 2017)
%

clear all, close all
format long e

%
% find coeffs for Case a with a1 = 2
A = [-1 0 1 0; 0 -2 1 2;-1 0 0 1;1 0 0 0];
b = [0 0 0 2]';
disp('Stoichiometric coeffs for Case a: '); a = A\b

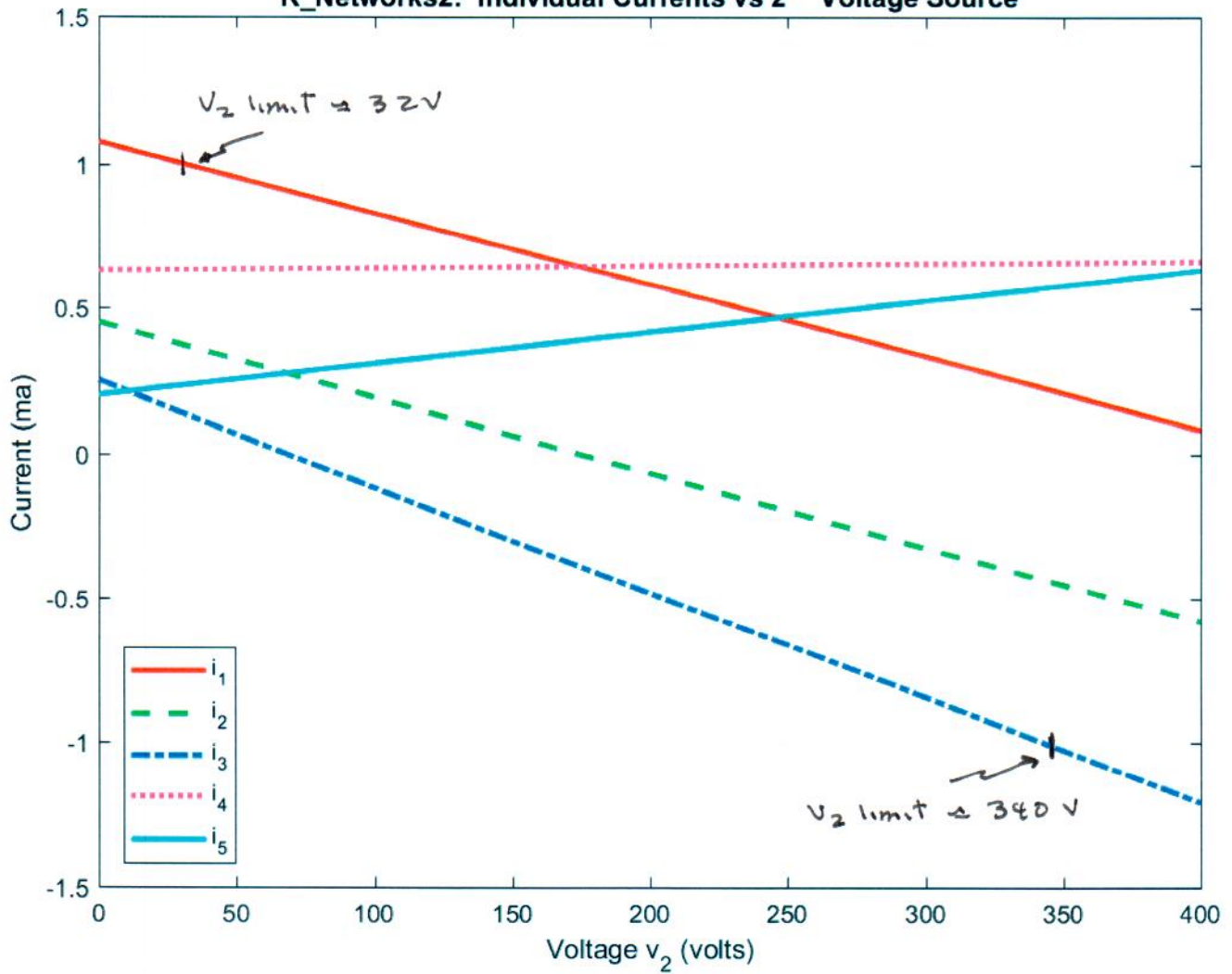
%
% find coeffs for Case b with a1 = 10
A = [ 0 -1 0 2 0 0 1 2 0; -7 0 0 2 0 0 0 0 0;
     -24 -4 -4 7 4 2 3 4 1; 0 -1 0 0 1 0 0 0 0;
      0 0 -1 0 1 0 0 1 0;-42 0 0 0 0 1 0 0 0;
     -66 0 0 0 0 0 1 0 0;-96 0 -2 0 0 0 0 0 2;
      1 0 0 0 0 0 0 0 0];
b = [0 0 0 0 0 0 0 0 10]';
disp('Stoichiometric coeffs for Case b: '); a = A\b

%
% end of problem

>> reaction_eqns1
Stoichiometric coeffs for Case a:
a =
     2
     3
     2
     2
Stoichiometric coeffs for Case b:
a =
 1.000000000000001e+01
 1.176000000000001e+03
 1.399000000000000e+03
 3.500000000000001e+01
 1.176000000000000e+03
 4.200000000000002e+02
 6.600000000000003e+02
 2.230000000000001e+02
 1.879000000000001e+03

```

R_Networks2: Individual Currents vs 2nd Voltage Source



∴ for $|i_i| < 1\text{ma}$ $32 < v_2 < 340$ volts


```
%
% RESISTIVE_NETWORKS2.M Find the currents and maximum allowed voltage range
% for a particular resistive network
```

```
% A resistive network is given along with the applied voltage for source #1.
% This file finds the allowed range of values (using graphical techniques) for a
% second voltage source such that the maximum current in the circuit is 1 ma.
% This requires solving a system of equations for each potential value of v2 and
% plotting the resulting currents versus v2. A point where any of the currents
% exceeds 1 ma represents a value of v2 that is not allowed. In this way, we
% should be able to easily visualize an appropriate range of values for v2.
```

```
% Concerning units, all the resistor values are given in k-ohm = 1000 ohm. Thus,
% since  $i = v/R$ , where v is in volts, the result will automatically be in
% milliamps (ma) if we use resistance in k-ohm and voltage in volts.
```

```
% Reference: This problem was derived from Prob. 24 in Chapter 4 of Palm's text,
% "Introduction to Matlab 6 for Engineers," McGraw Hill (2001).
```

```
% File prepared by J. R. White, UMass-Lowell (last update: Nov. 2017)
```

```
clear all, close all
```

```
% define given problem parameters
```

```
R = [5 100 200 150 250]; % resistances (k-ohm)
v1 = 100; % voltage source #1 (volts)
```

```
% set potential range for second voltage source
```

```
Nv2 = 101; v2 = linspace(0,400,Nv2)';
```

```
% start loop over number of voltage values
```

```
cur = zeros(Nv2,5); % initialize 2-D matrix for results
A = [R(1) 0 0 R(4) 0 ; % coeff matrix (independent of v2)
     0 R(2) 0 -R(4) R(5);
     0 0 R(3) 0 -R(5);
     1 -1 0 -1 0 ;
     0 1 -1 0 -1 ];
```

```
for j = 1:Nv2
```

```
    b = [v1 0 -v2(j) 0 0]'; % RHS vector for specific v2
    I = A\b; % solve for current vector in ma
    cur(j,:) = I'; % store currents in jth row of 2-D matrix
end
```

```
% let's plot the results to visualize the allowed range for v2
```

```
plot(v2,cur(:,1),'r-',v2,cur(:,2),'g--',v2,cur(:,3),'b-. ',...
     v2,cur(:,4),'m:',v2,cur(:,5),'c-', 'LineWidth',2),grid
xlabel('Voltage v_2 (volts)'),ylabel('Current (ma)')
title('R\ Networks2: Individual Currents vs 2^{nd} Voltage Source')
legend('i_1','i_2','i_3','i_4','i_5','Location','SouthWest')
```

```
% end of problem
```

Consider heat conduction through the wall of a circular pipe. The inside wall temperature is 200°C and the outside wall temperature is 80°C . The inner radius of the pipe is $a = 0.05\text{ m}$ and the outer radius is $b = 0.1\text{ m}$.

The differential eqn which describes the temperature distribution in the pipe is

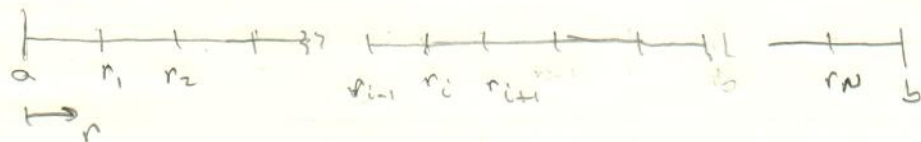
$$\frac{d^2 T}{dr^2} + \frac{1}{r} \frac{dT}{dr} = 0$$

with boundary conditions

$$T(a) = 200 \quad \text{and} \quad T(b) = 80$$

Although this boundary value problem (BVP) can be solved analytically, here you will develop a numerical solution (see the Example Application "Introduction to Finite Difference Methods" in the notes for Lesson #4).

One always starts by discretization of the independent variable. Recognizing ^{that} the temperatures at the inner and outer surfaces are known, we have the following 1-D discrete representation of the spatial grid for this problem



where r_i represents the radius of the i^{th} discrete unknown temperature, T_i . The vector of spatial grids can be generated within matlab as follows

$$N = \# \text{ of unknown Temperature in domain (interior)}$$

$$h = \Delta r = \frac{b - a}{N + 1} = \text{step size}$$

$$r = a + h : h : b - h = \text{vector of locations for unknown temperatures}$$

Now, using 2nd order central finite difference (FD) approximations for the derivatives

$$\left. \frac{d^2 T}{dr^2} \right|_i = \frac{T_{i-1} - 2T_i + T_{i+1}}{h^2}$$

and

$$\left. \frac{dT}{dr} \right|_i = \frac{T_{i+1} - T_{i-1}}{2h}$$

formally develop the discrete FD equations needed for this problem, being careful to treat the boundary nodes as special cases (i.e. when $i=1$ and $i=N$). the final result should be as follows:

central node

$$\left. \frac{d^2 T}{dr^2} \right|_i + \frac{1}{r} \left. \frac{dT}{dr} \right|_i = 0$$

$$\frac{T_{i-1} - 2T_i + T_{i+1}}{h^2} + \frac{1}{r_i} \frac{T_{i+1} - T_{i-1}}{2h} = 0$$

$$T_{i-1} - 2T_i + T_{i+1} + \frac{h}{2r_i} (T_{i+1} - T_{i-1}) = 0$$

$$\left(1 - \frac{h}{2r_i}\right) T_{i-1} - 2T_i + \left(1 + \frac{h}{2r_i}\right) T_{i+1} = 0 \quad i = 2 : N-1$$

node 1

simply set $i=1$

$$-2T_1 + \left(1 + \frac{h}{2r_1}\right) T_2 = -\left(1 - \frac{h}{2r_1}\right) T(a)$$

node N

simply set $i=N$

$$\left(1 - \frac{h}{2r_N}\right) T_{N-1} - 2T_N = -\left(1 + \frac{h}{2r_N}\right) T(b)$$

b) Now, implement the discrete eqns developed in Part a along with the discrete geometry information and actually solve the resultant matrix equations, $\underline{AT} = \underline{B}$, for the unknown discrete temperature profile, T , within the pipe. Plot the temperature profile (including the two known end-point temperatures) for this problem. Does your solution make sense? Are the boundary conditions (BCs) satisfied by your solution?

$$\begin{aligned} \frac{d}{dr} \left(\frac{dT}{dr} \right) + \frac{1}{r} \frac{dT}{dr} &= 0 \\ \frac{d}{dr} (T') &= -\frac{1}{r} T' \\ \frac{dT'}{T'} &= -\frac{1}{r} dr \\ \ln T' &= -\ln r + \ln C_1 \\ T' &= C_1/r \end{aligned}$$

c) The analytical soln to this problem is given by

$$T(r) = C_1 \ln r + C_2$$

$$\left\{ \begin{aligned} dT &= \frac{C_1}{r} dr \\ T(r) &= C_1 \ln r + C_2 \end{aligned} \right.$$

where C_1 and C_2 are constants that are chosen to satisfy the given BCs, i.e.

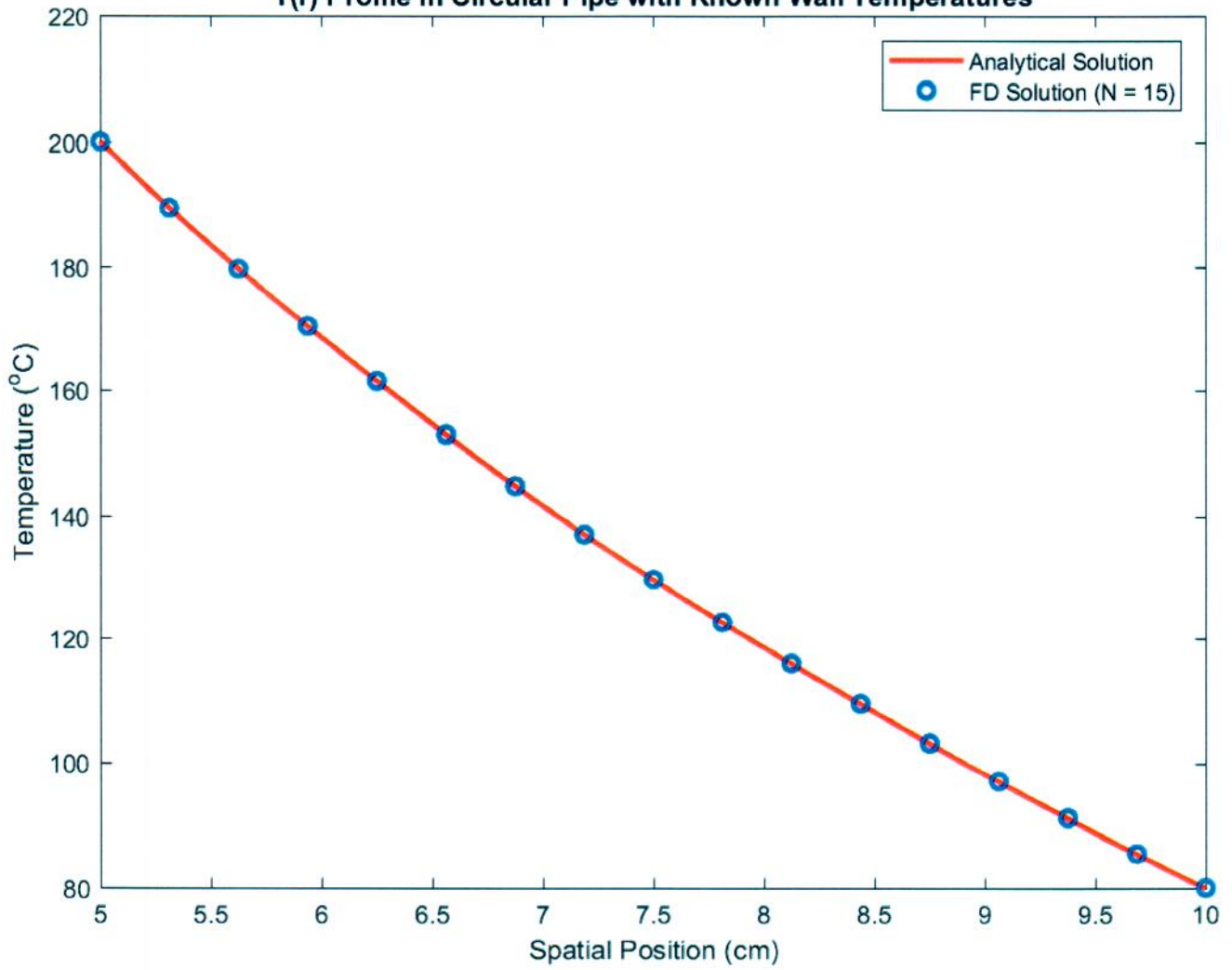
$$T(a) = C_1 \ln a + C_2$$

$$T(b) = C_1 \ln b + C_2$$

see htprob-fd1.0.m

Evaluate and plot this exact solution for the conditions given above. Does the FD solution from Part b compare favorably? Explain any differences.

T(r) Profile in Circular Pipe with Known Wall Temperatures



```

%
% HTPROB_FD1.M Introduction to FD Methods for Solving BVPs
% Heat Conduction through a thick Circular Pipe
%
% This file illustrates the finite difference (FD) method for solving BVPs.
% We solve a simple heat transfer problem that involves heat conduction in a thick
% circular pipe with known temperatures at the inner and outer radius of the pipe.
% For comparison, we also evaluate the analytical solution -- showing that the
% two methods give identical solutions.
%
% File prepared by J. R. White, UMass-Lowell (last update: Nov. 2017)
%

clear all, close all, nfig = 0;

%
% identify basic problem data
a = 0.05; b = 0.1; % inner and outer radii of pipe (m)
Ta = 200; Tb = 80; % boundary temperatures (C)
%
%% Analytical Solution
%
Nr = 51; re = linspace(a,b,Nr)'; % independent variable
Ae = [log(a) 1;log(b) 1]; Be = [Ta Tb]'; c = Ae\Be; % coeffs in exact soln
Te = c(1)*log(re) + c(2); % exact soln
%
%% FD Solution
%
% setup and solve matrix eqn for discrete temperatures
N = input('Enter number of discrete unknowns (N) for problem: ');
h = (b-a)/(N+1); rn = a+h:h:b-h; rn = rn';
A = zeros(N,N); B = zeros(N,1);
%
% node 1
A(1,1) = -2; A(1,2) = 1 + h/(2*rn(1)); B(1) = -(1 - h/(2*rn(1)))*Ta ;
%
% interior nodes
for i = 2:N-1
    A(i,i-1) = 1 - h/(2*rn(i)); A(i,i) = -2; A(i,i+1) = 1 + h/(2*rn(i));
end
%
% last node
A(N,N-1) = 1 - h/(2*rn(N)); A(N,N) = -2; B(N) = -(1 + h/(2*rn(N)))*Tb;
%
% solve
Tn = A\B;
%
% add on the known endpoint temperatures to the solution vector
rnp = [a; rn; b]; Tnp = [Ta; Tn; Tb];
%
%% plot both solutions
nfig = nfig+1; figure(nfig)
plot(re*100,Te,'r-',rnp*100,Tnp,'bo','LineWidth',2),grid
title('T(r) Profile in Circular Pipe with Known Wall Temperatures')
xlabel('Spatial Position (cm)')
ylabel('Temperature (^oC)')
legend('Analytical Solution',['FD Solution (N = ',num2str(N),')'])
%
end of problem

```