

CHEN.3030 Fluid Mechanics

VII. Internal Viscous Flows

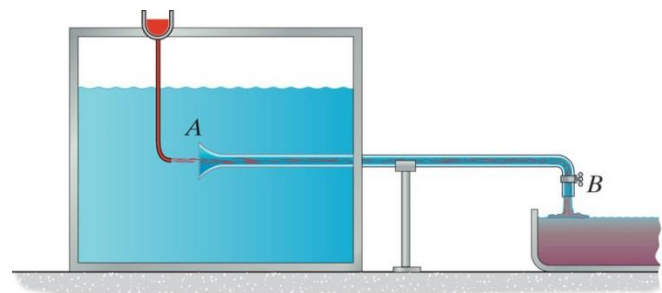
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See Chapter 9
(all sections except
9.2 & 9.4) in your
text by Hibbeler

Laminar vs. Turbulent Flow



(a)

$$\text{Re} = \frac{\rho v L}{\mu} = \frac{v L}{\nu}$$

where L is a **characteristic dimension** associated with the flow geometry

$L \rightarrow D =$ pipe diameter for pipe flow

$L \rightarrow D_h =$ hydraulic diameter for general internal flows



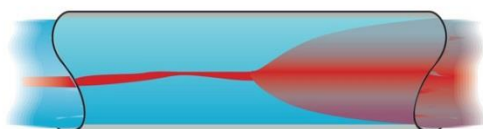
Laminar flow

(b)



Transitional flow

(c)



Turbulent flow

(d)

$$D_h = \frac{4A_f}{P_w}$$

where A_f is the flow area and P_w is the wetted perimeter

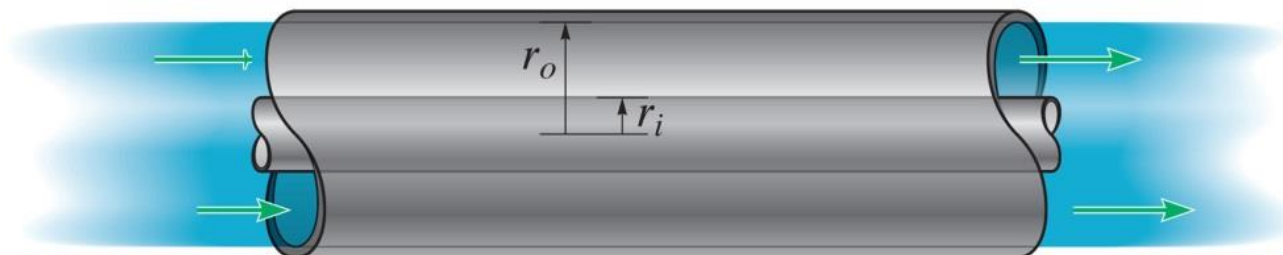
Ex. #1 -- hydraulic diameter...

Consider water flow within the annulus shown in the sketch for $T = 30\text{ }^{\circ}\text{C}$ and $Q = 0.01\text{ m}^3/\text{s}$ with $r_i = 0.04\text{ m}$ and $r_o = 0.06\text{ m}$.

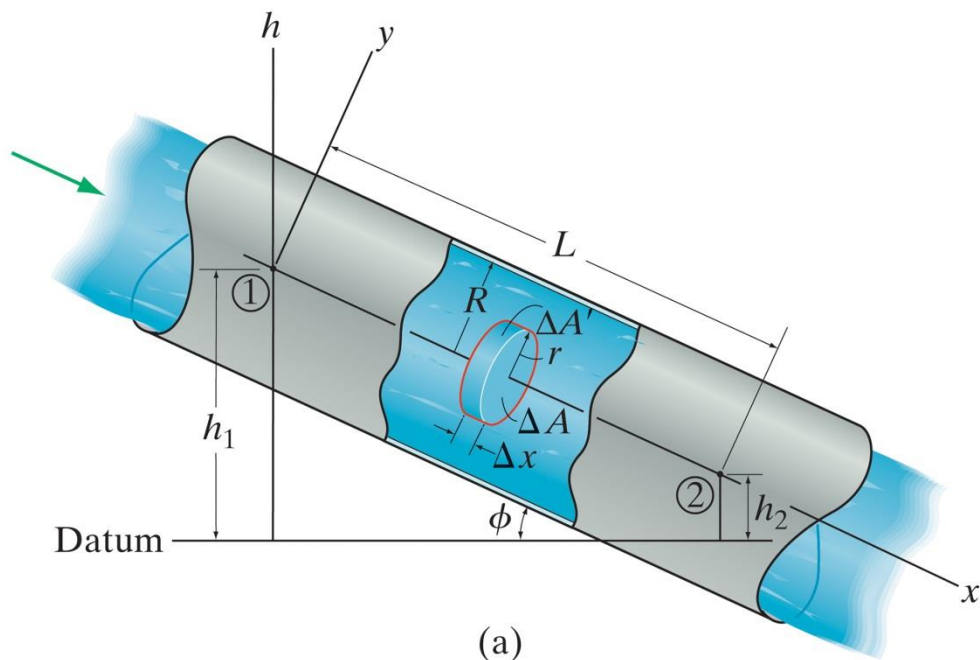
Is the flow laminar or turbulent?

Water properties at $30\text{ }^{\circ}\text{C}$ from Appendix A :

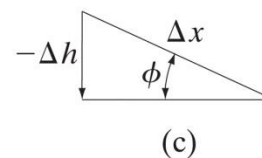
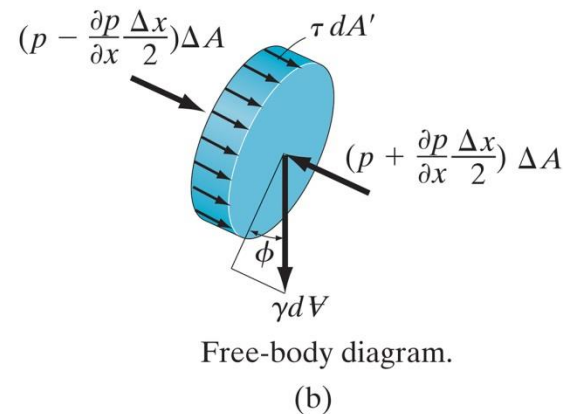
$$\rho = 995.7\text{ kg/m}^3 \quad \text{and} \quad \mu = 0.801 \times 10^{-3}\text{ N}\cdot\text{s/m}^2$$



Steady Laminar Flow – Smooth Pipe



**Basic Configuration and
Coordinate Definitions**



Free Body Diagram

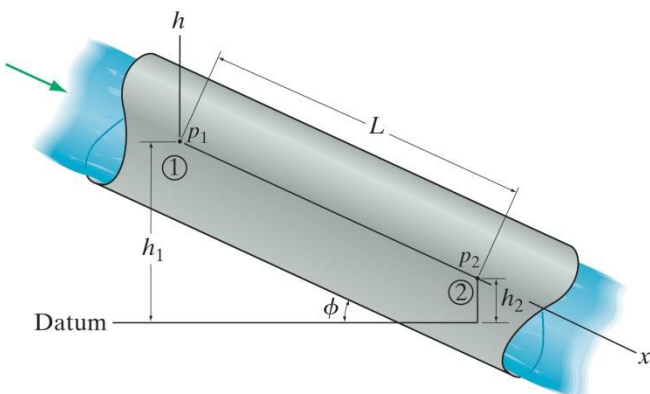
Steady Laminar Flow – Smooth Pipe

$$\tau(r) = \frac{r}{2} \frac{d}{dx} (P + \gamma h)$$

Shear Stress Distribution
(Laminar + Turbulent)

$$u(r) = -\frac{(R^2 - r^2)}{4\mu} \frac{d}{dx} (P + \gamma h)$$

Velocity Profile
(Laminar Flow Only)



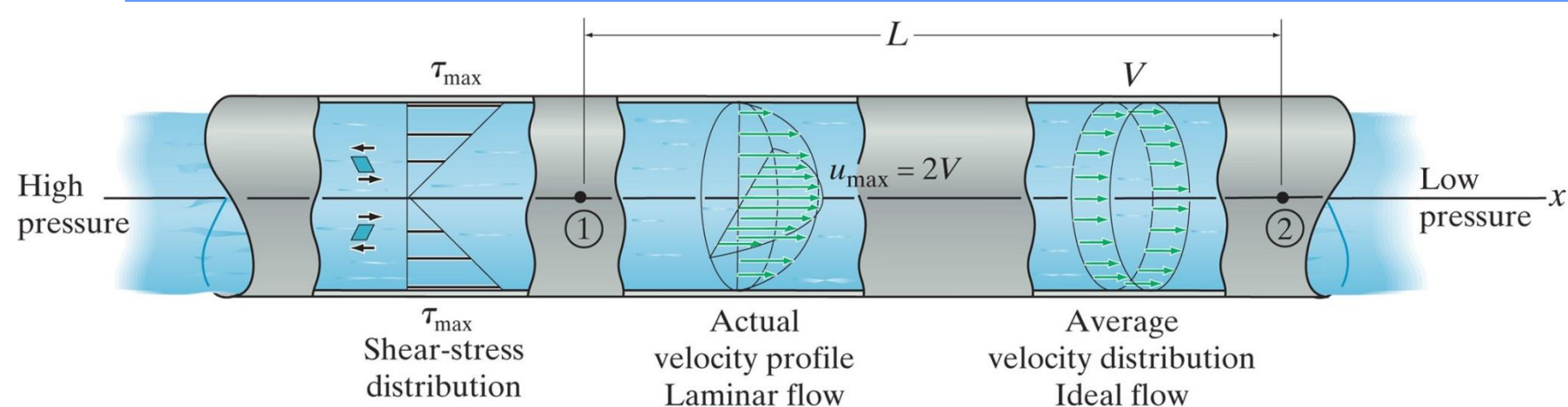
or

$$\frac{d}{dx} (P + \gamma h) = \frac{P_2 - P_1}{L} + \gamma \frac{h_2 - h_1}{L}$$

$$-\frac{d}{dx} (P + \gamma h) = \frac{P_1 - P_2}{L} + \gamma \frac{h_1 - h_2}{L}$$

Pressure and Elevation Gradients

Steady Laminar Flow – Smooth Pipe



Shear Stress and Velocity Profile for a Negative Pressure Gradient

Also
$$Q = \int_A \vec{v} \cdot \hat{n} \, dA = \int_A u \, dA = -\frac{\pi D^4}{128\mu} \frac{d}{dx} (P + \gamma h)$$

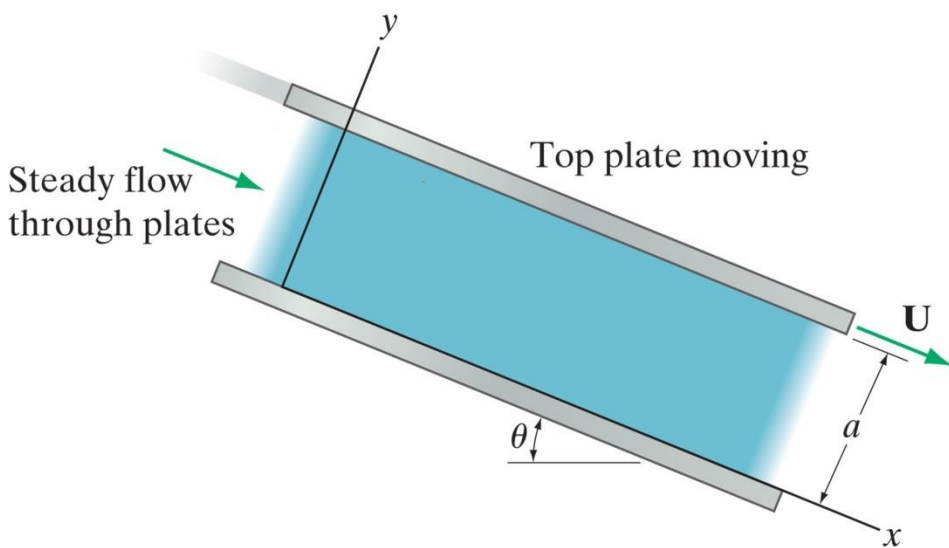
and
$$-\frac{d}{dx} (P + \gamma h) = \frac{\gamma h_L}{L}$$

from Energy Eqn.

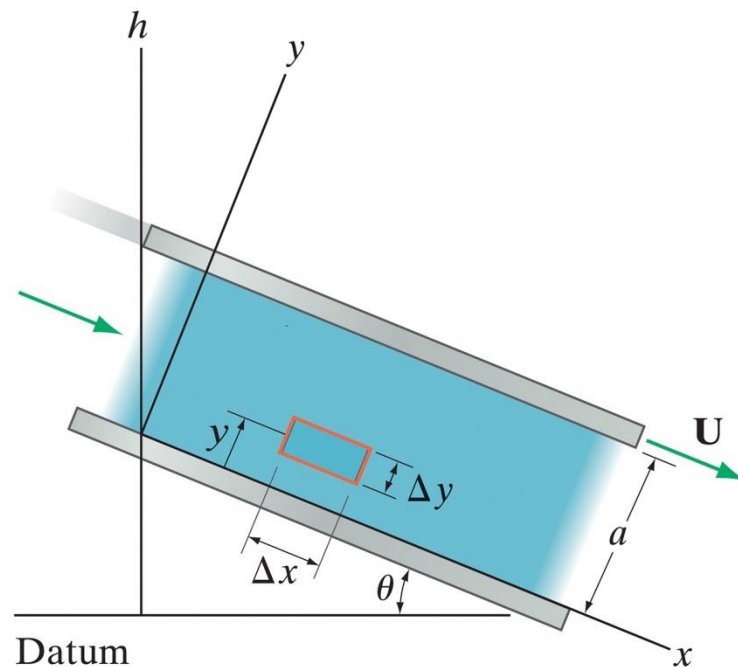
Thus,

$$h_L = \frac{128\mu L Q}{\rho g \pi D^4} = \frac{32\mu L v}{\rho g D^2}$$

Steady Laminar Flow – Parallel Plates

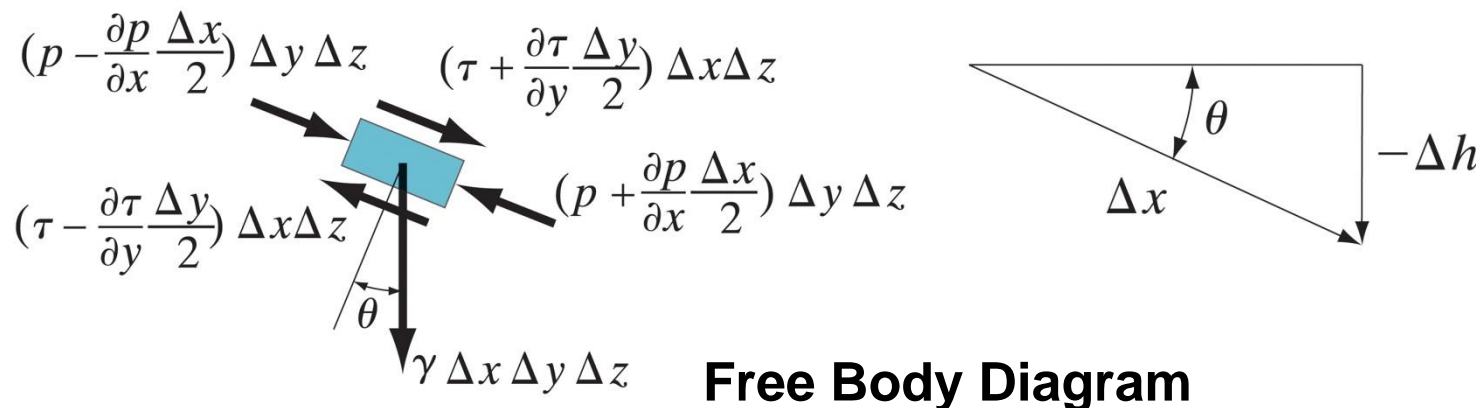


Basic Configuration



Coordinate Definitions

Steady Laminar Flow – Parallel Plates



$$\tau(y) = \frac{U\mu}{a} + \left[\frac{d}{dx} (P + \gamma h) \right] \left(y - \frac{a}{2} \right)$$

**Shear Stress
Distribution**
(Laminar + Turbulent)

$$u(y) = \frac{U}{a} y - \frac{1}{2\mu} \left[\frac{d}{dx} (P + \gamma h) \right] (ay - y^2)$$

**Velocity
Profile**
(Laminar Flow Only)

Steady Laminar Flow – Parallel Plates

Note that the above development used the fact that the **sum of the pressure and elevation gradients are independent of y!!!**

$$\frac{d}{dx}(P + \gamma h) = \frac{P_2 - P_1}{L} + \gamma \frac{h_2 - h_1}{L}$$

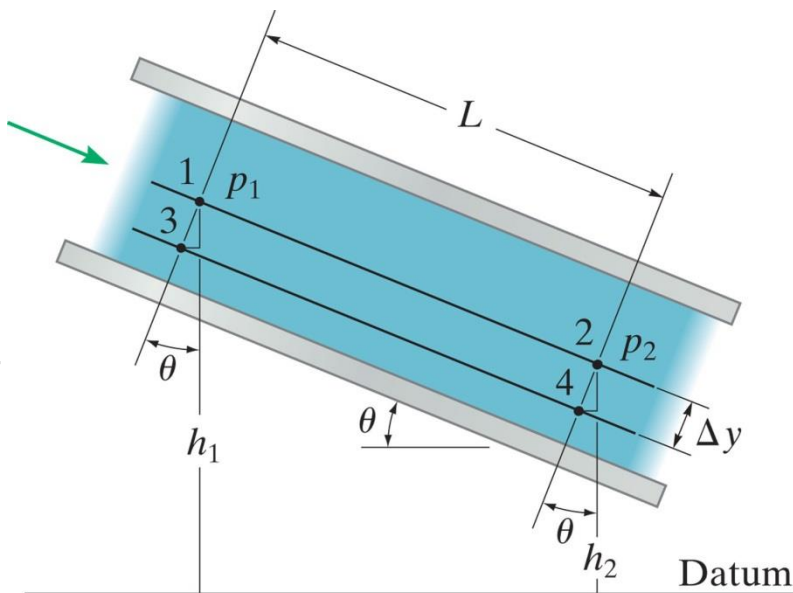
or

$$\frac{d}{dx}(P + \gamma h) = \frac{P_4 - P_3}{L} + \gamma \frac{h_4 - h_3}{L}$$

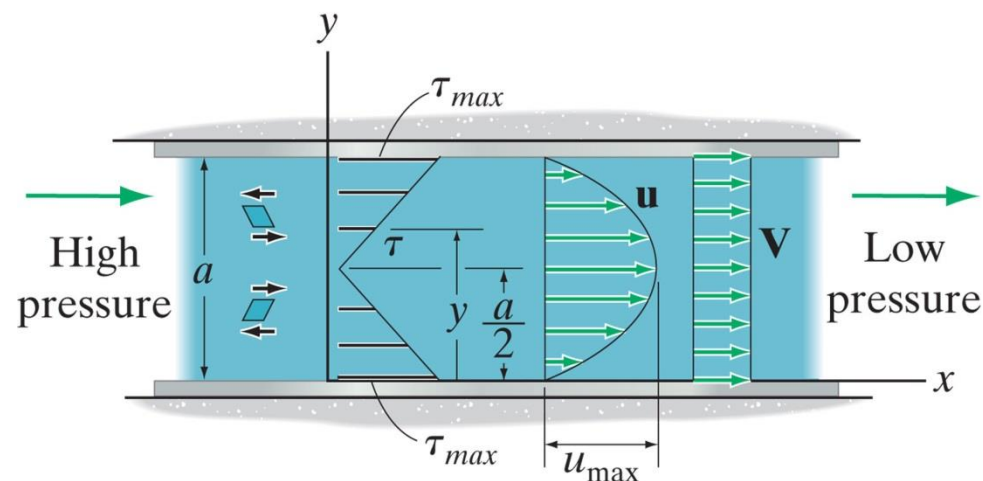
(see discussion in Hibbeler pg. 471)

and

$$-\frac{d}{dx}(P + \gamma h) = \frac{P_1 - P_2}{L} + \gamma \frac{h_1 - h_2}{L}$$



Steady Laminar Flow – Parallel Plates



Shear-stress distribution and actual and average velocity profiles with *negative* pressure gradient and no motion of the plates.

For $U = 0$ (no plate movement) and $b =$ plate depth into page, we have

$$Q = \int_A \vec{v} \cdot \hat{n} dA = \int_A u dA$$

$$= -\frac{ba^3}{12\mu} \frac{d}{dx} (P + \gamma h)$$

and **from Energy Eqn.**

$$-\frac{d}{dx} (P + \gamma h) = \frac{\gamma h_L}{L}$$

Thus,

$$h_L = \frac{12\mu L Q}{\rho g b a^3} = \frac{12\mu L v}{\rho g a^2}$$

Steady Laminar Flow – Darcy Eqn.

Circular Pipe

$$h_L = \frac{128\mu L Q}{\rho g \pi D^4} = \frac{32\mu L v}{\rho g D^2}$$

$$D_h = \frac{4(\pi D^2/4)}{\pi D} = D$$

$$h_L = (32)(2) \frac{\mu}{\rho v D} \frac{L}{D} \frac{v^2}{2g}$$

$$h_L = \frac{64}{\text{Re}} \frac{L}{D} \frac{v^2}{2g}$$

$$D_h = \frac{4A_f}{P_w}$$

$$h_L = f \frac{L}{D_h} \frac{v^2}{2g}$$

Darcy Eqn.

Parallel Plates ($b \gg a$)

$$h_L = \frac{12\mu L Q}{\rho g b a^3} = \frac{12\mu L v}{\rho g a^2}$$

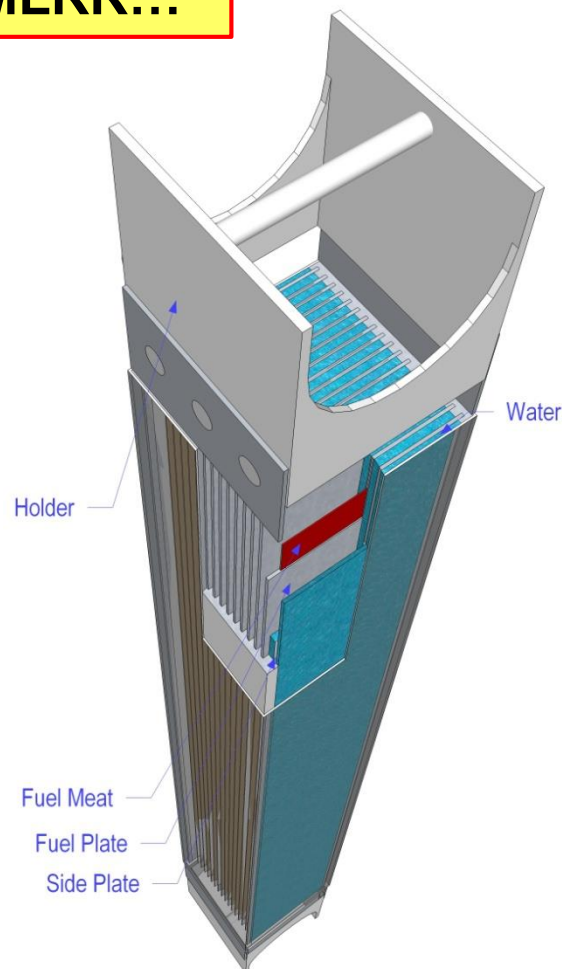
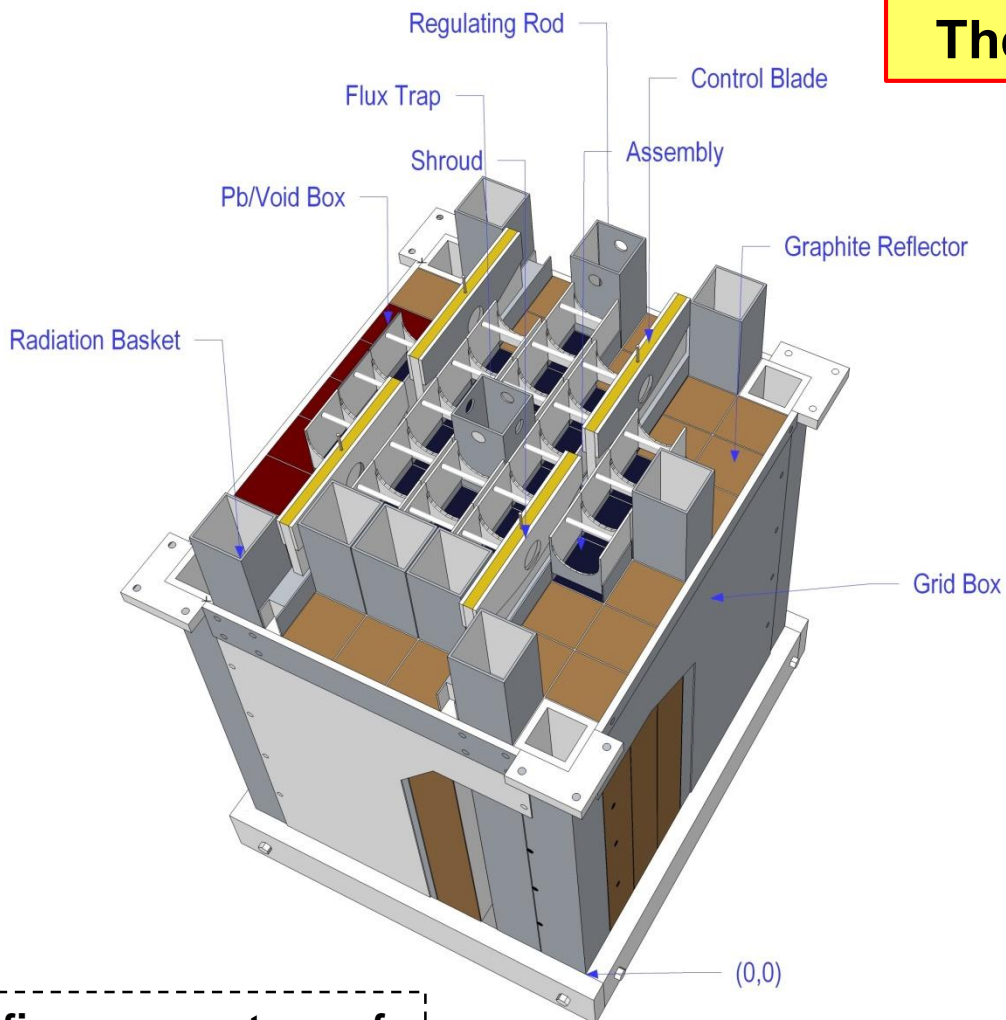
$$D_h = \frac{4ab}{2a + 2b} \approx 2a$$

$$h_L = (12)(8) \frac{\mu}{\rho v 2a} \frac{L}{2a} \frac{v^2}{2g}$$

$$h_L = \frac{96}{\text{Re}_h} \frac{L}{D_h} \frac{v^2}{2g}$$

Ex. #2 -- ΔP in MTR Fuel

The UMLRR...



figures courtesy of
Mr. Odera Dim

Ex. #2 (continued)

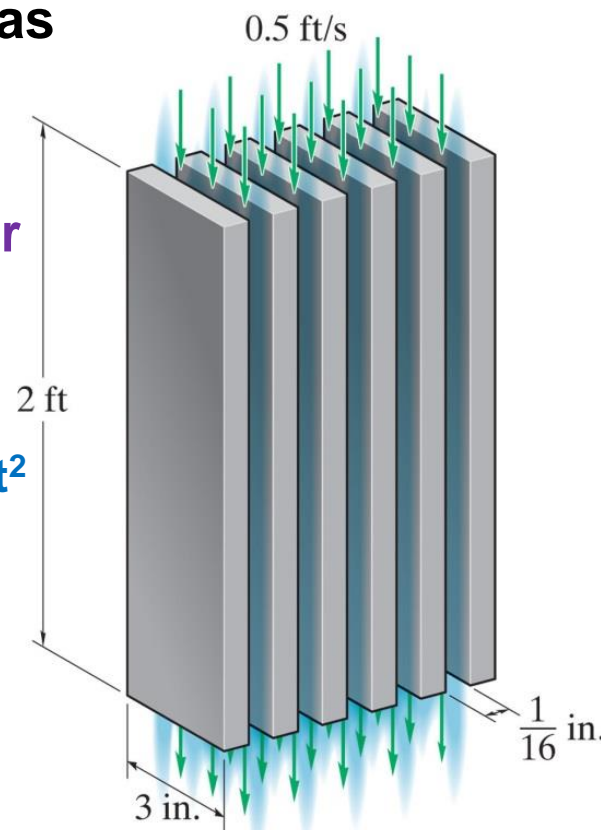
Consider the MTR fuel plate flow geometry as shown.

Water flows downward between the plates.

Neglecting end effects, estimate the ΔP over the 2 ft length of the fuel plates.

water properties:

$$\rho = 1.820 \text{ slugs/ft}^3 \quad \& \quad \mu = 5.46 \times 10^{-6} \text{ lbf-s/ft}^2$$



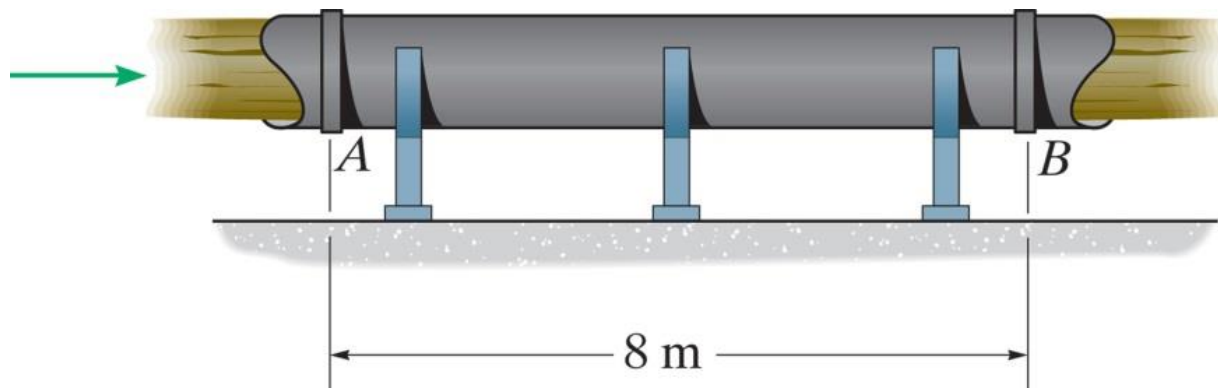
Ex. #3 -- ΔP and head Loss...

Oil has a flow rate $Q = 0.004 \text{ m}^3/\text{s}$ through the 0.15 m diameter pipe.

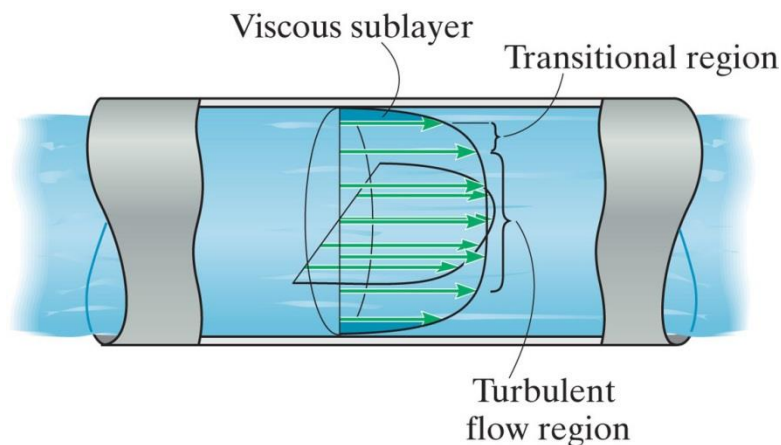
Determine the pressure drop in the 8-m long section and calculate the head loss per meter of pipe.

oil properties:

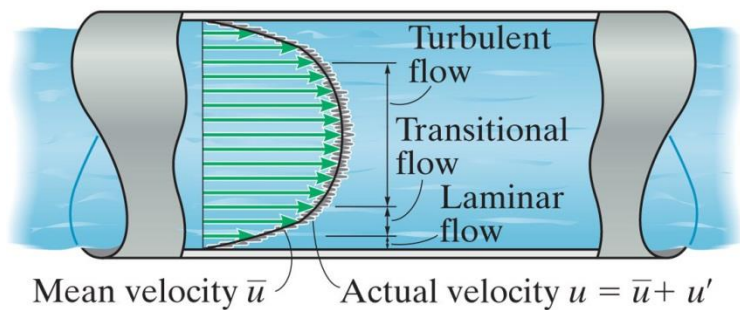
$$\rho = 900 \text{ kg/m}^3 \quad \text{and} \quad \mu = 0.370 \text{ N-s/m}^2$$



Fully Developed Turbulent Flow

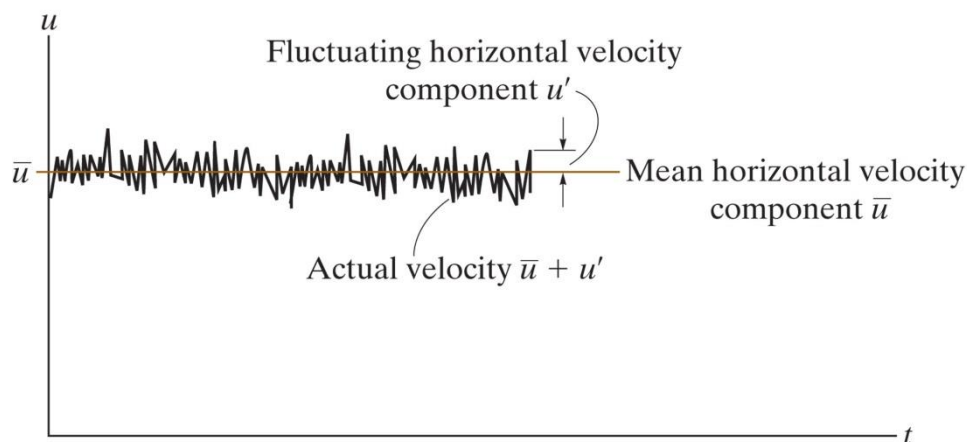


(a)



Mean velocity \bar{u} (solid line)
Actual velocity $u = \bar{u} + u'$

(b)



Horizontal velocity components of fluid particles passing through a control volume.

Fully Developed Turbulent Flow

Dimensionless Velocity fit to Experimental Data

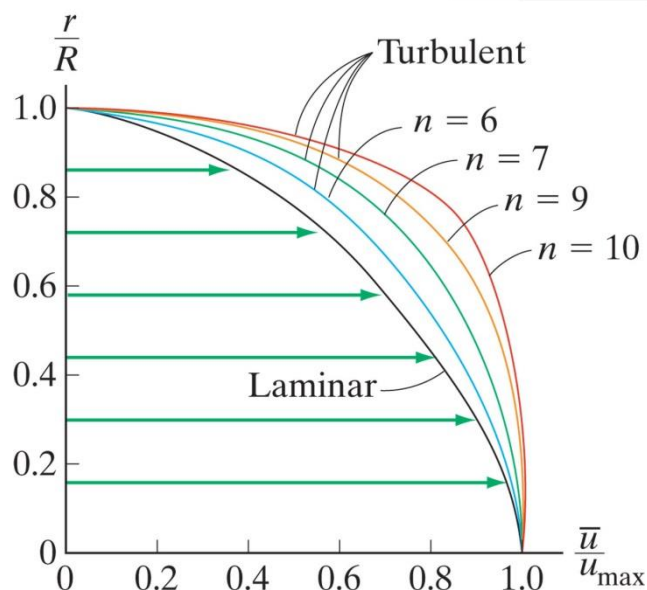
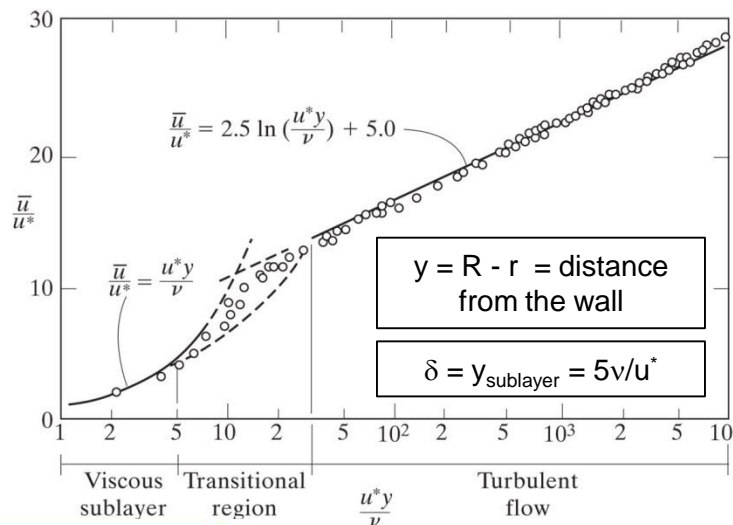
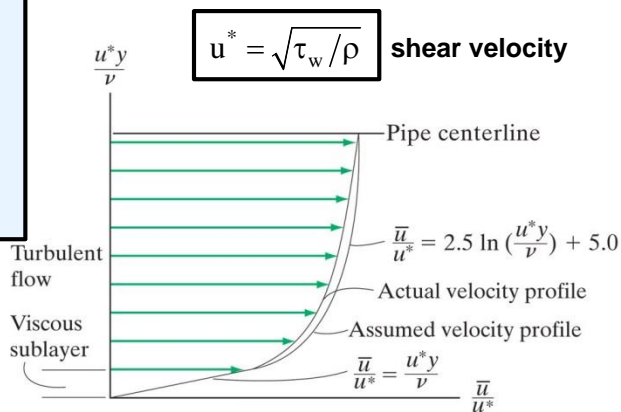


TABLE 9-1

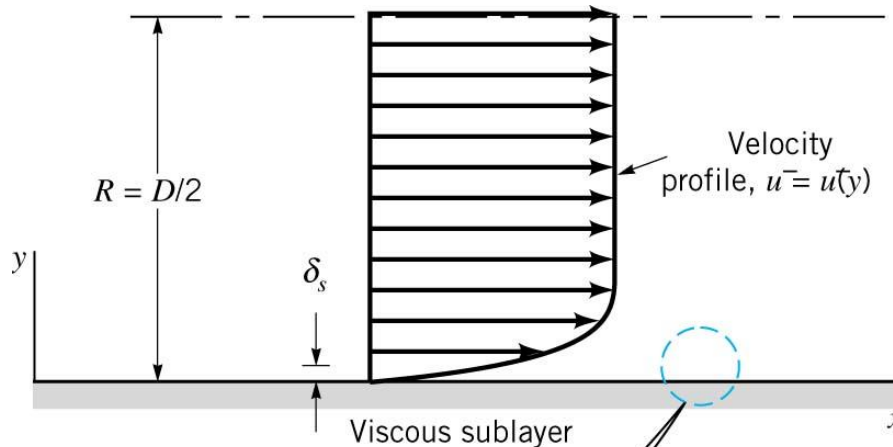
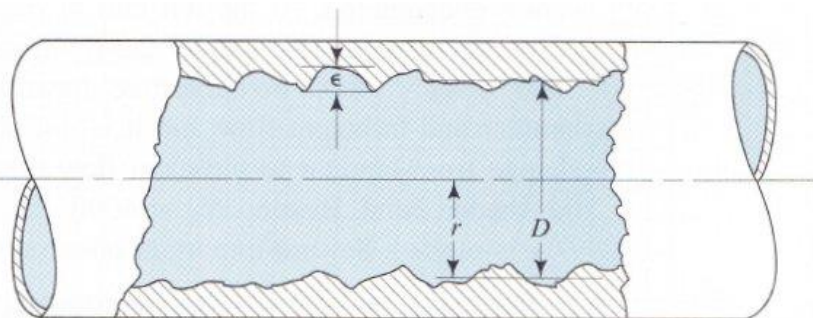
n	Re
6	4 (10^3)
7	1 (10^5)
9	1 (10^6)
10	3 (10^6)

$$u(y) = u_{\text{max}} \left(\frac{y}{R}\right)^{1/n}$$

$$u(r) = u_{\text{max}} \left(1 - \frac{r}{R}\right)^{1/n}$$

Power Law Model

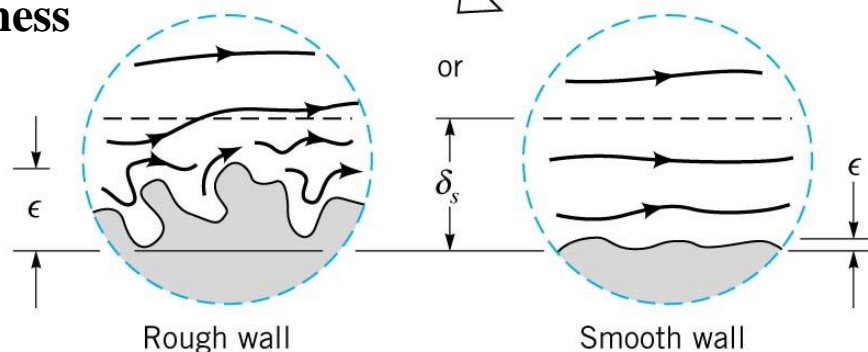
Surface Roughness



$$h_L = f \frac{L}{D_h} \frac{v^2}{2g}$$

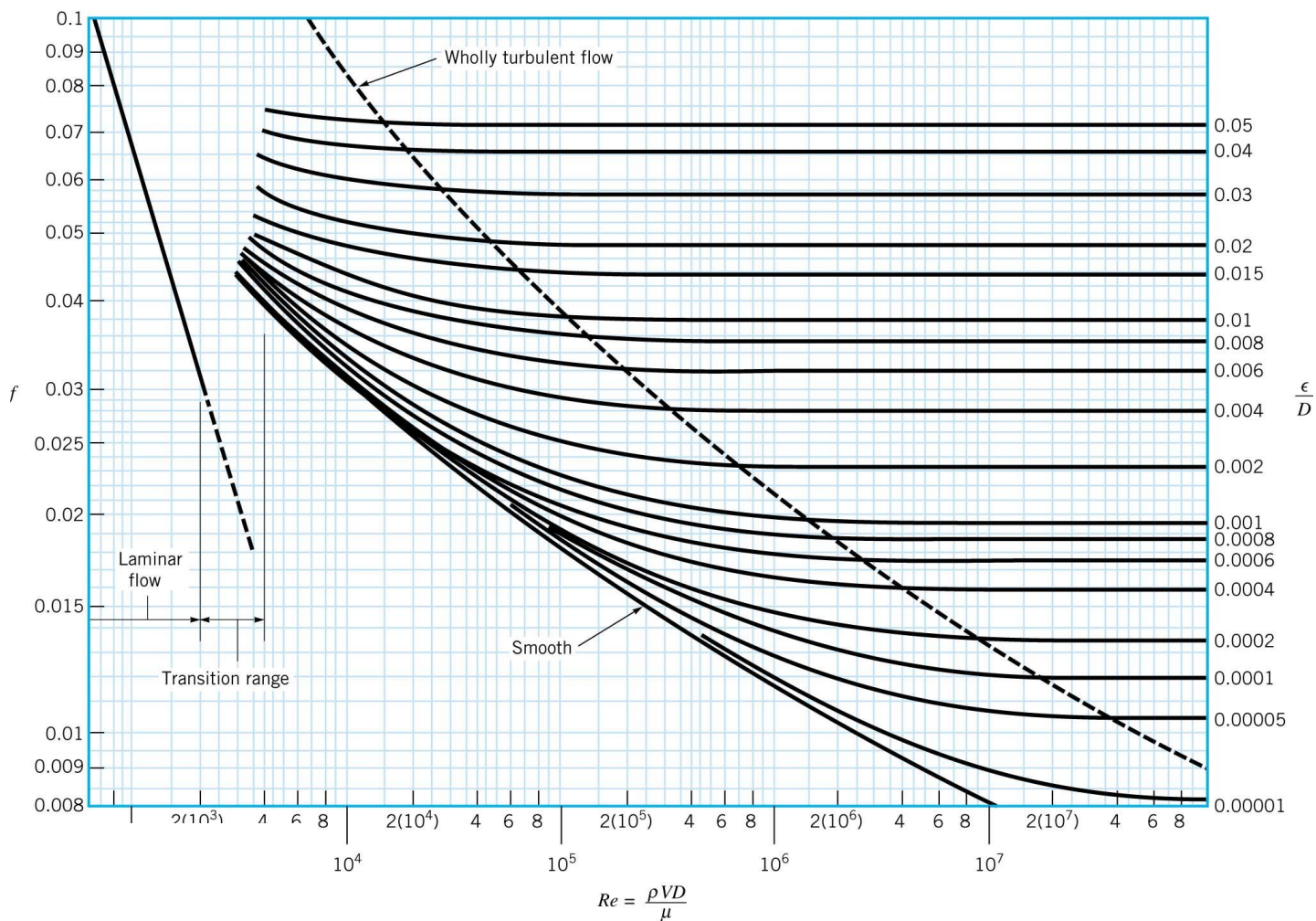
$$f = \phi\left(\frac{\epsilon}{D}, Re\right)$$

where $\epsilon/D =$ relative roughness



Material	Roughness ϵ (m)	Roughness ϵ (ft)
Glass	Smooth	Smooth
Plastic	3.0×10^{-7}	1.0×10^{-6}
Drawn tubing; copper, brass, steel	1.5×10^{-6}	5.0×10^{-6}
Steel, commercial or welded	4.6×10^{-5}	1.5×10^{-4}
Galvanized iron	1.5×10^{-4}	5.0×10^{-4}
Ductile iron—coated	1.2×10^{-4}	4.0×10^{-4}
Ductile iron—uncoated	2.4×10^{-4}	8.0×10^{-4}
Concrete, well made	1.2×10^{-4}	4.0×10^{-4}
Riveted steel	1.8×10^{-3}	6.0×10^{-3}

The Moody Chart (preview from Chapter 10)



Ex. #4 -- Turbulent Flow ...

Water flows in the 2-in diameter smooth pipe with $\Delta P = 1.5$ psi along the 2-ft length.

Determine the shear stress along the wall and at the pipe centerline. Also compute u_{\max} .

water properties:

$$\rho = 62.4 \text{ lbm/ft}^3 \quad \text{and} \quad \nu = 16.6 \times 10^{-6} \text{ ft}^2/\text{s}$$

