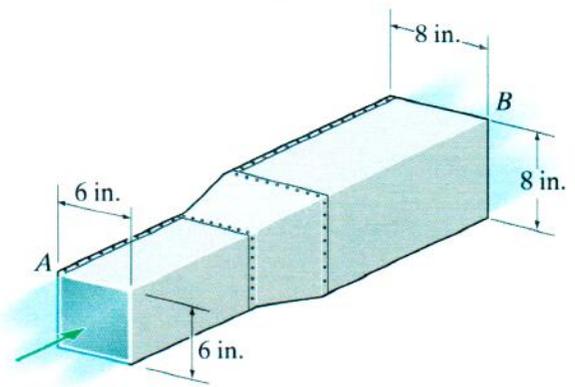


Air at 100 °F flows through the square horizontal duct section at Point A at 200 ft/s under a pressure of 1.50 psi.

Determine the pressure in the square duct section at Point B.



Write Bernoulli Eqn from A to B

$$\frac{P_A}{\gamma} + \frac{V_A^2}{2g} + z_A = \frac{P_B}{\gamma} + \frac{V_B^2}{2g} + z_B$$

- $z_A = z_B$
- $P_A = 1.50 \text{ psi}$
- $V_A = 200 \text{ ft/s}$
- assume
- ① incompressible
- ② no friction

$$P_B = P_A + \frac{\gamma}{2g} (V_A^2 - V_B^2)$$

$$P_B = P_A + \frac{\rho}{2} (V_A^2 - V_B^2)$$

But from the continuity eqn for incompressible flow

$$Q_A = Q_B$$

$$V_A A_A = V_B A_B \Rightarrow V_B^2 = V_A^2 \left( \frac{A_A}{A_B} \right)^2$$

$$\therefore P_B = P_A + \frac{\rho}{2} \left( 1 - \frac{A_A^2}{A_B^2} \right) V_A^2$$

$$A_A^2 = (36 \text{ in}^2)^2 = 1296 \text{ in}^4$$

$$A_B^2 = (64 \text{ in}^2)^2 = 4096 \text{ in}^4$$

Now let's insert the values

$$\rho_{\text{air}} = 0.00220 \frac{\text{slugs}}{\text{ft}^3}$$

$$P_B = 1.50 \frac{\text{lb}}{\text{in}^2} + \left( \frac{0.00220 \text{ slugs}}{2 \text{ ft}^3} \right) \left( 1 - \frac{1296}{4096} \right) \left( 200 \frac{\text{ft}}{\text{s}} \right)^2$$

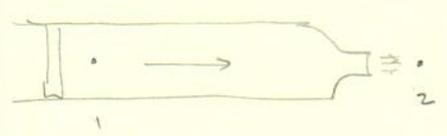
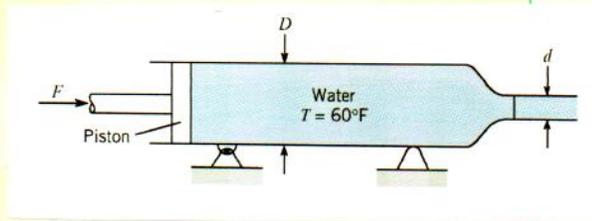
$$= 1.50 \frac{\text{lb}}{\text{in}^2} + 30.08 \frac{\text{lb}}{\text{ft}^2} \times \frac{1 \text{ ft}^2}{144 \text{ in}^2}$$

$$= 1.50 + 0.209$$

or  $P_B \approx 1.71 \text{ psi}$  ans

Hibbeler  
 Prob A

5.52 Water is forced out of the cylinder shown in the diagram. If the piston is driven at a speed of 4 ft/s, what will be the average exit velocity of the water if  $d = 2$  in and  $D = 4$  in? Also estimate the force that will be required to drive the piston.



Bernoulli eqn from ① to ②

$$\frac{P_1}{\rho} + \frac{V_1^2}{2g} + z_1 = \frac{P_2}{\rho} + \frac{V_2^2}{2g} + z_2$$

horizontal

$$\therefore \frac{P_1}{\rho} = \frac{V_2^2 - V_1^2}{2g}$$

Continuity Eqn

$$Q_1 = Q_2 \quad \therefore V_2 = \frac{V_1 A_1}{A_2} = \frac{(4 \text{ ft/s}) \frac{\pi}{4} (4 \text{ in})^2}{\frac{\pi}{4} (2 \text{ in})^2}$$

$$V_2 = 16 \text{ ft/s} \quad \text{ans}$$

now putting this into the Bernoulli Eqn

$$P_1 = \frac{\rho (V_2^2 - V_1^2)}{2} = \frac{1.94 \text{ slug} \cdot \text{ft}^{-3}}{2} (16^2 - 4^2) \text{ ft}^2/\text{s}^2$$

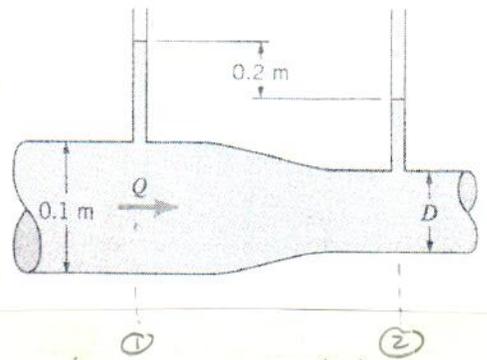
$$1 \text{ lbf} = 1 \text{ slug} \frac{\text{ft}}{\text{s}^2}$$

$$= 232.8 \frac{\text{slug} \cdot \text{ft}}{\text{ft} \cdot \text{s}^2} \left( \frac{\text{ft}}{\text{ft}} \right) = 232.8 \frac{\text{lbf}}{\text{ft}^2} \times \frac{1 \text{ ft}^2}{144 \text{ in}^2}$$

$$P_1 = 1.62 \text{ psi}$$

$$\therefore F_1 = P_1 A_1 = \left( 1.62 \frac{\text{lbf}}{\text{in}^2} \right) \left( \frac{\pi}{4} (4 \text{ in})^2 \right) = 20.3 \text{ lbf} \quad \text{ans}$$

3.31 Water flows through the pipe contraction as shown. For the given 0.2 m difference in the manometer level, determine the flow rate,  $Q$ , in the pipe if  $D = 0.05$  m. Neglect viscous effects.



First identify the upstream and downstream locations of the manometer tubes as pt 1 and pt 2.

Now applying the Bernoulli eqn., we have

$$\frac{P_1}{\gamma} + \frac{V_1^2}{2g} + z_1 = \frac{P_2}{\gamma} + \frac{V_2^2}{2g} + z_2 \quad \left\{ \text{where } z_1 = z_2 = 0 \right.$$

thus, 
$$\frac{P_1 - P_2}{\gamma} = \frac{V_2^2 - V_1^2}{2g}$$

From the continuity eqn

$$Q_1 = Q_2 \quad \Rightarrow \quad A_1 V_1 = A_2 V_2 \quad \Rightarrow \quad V_2 = \frac{A_1}{A_2} V_1 = \left( \frac{D_1}{D_2} \right)^2 V_1$$

Putting this result into the reduced Bernoulli eqn gives

$$\frac{\left[ \left( \frac{D_1}{D_2} \right)^4 - 1 \right] V_1^2}{2g} = \frac{P_1 - P_2}{\gamma}$$

$$\text{or } V_1 = \left[ \frac{2g(P_1 - P_2)}{\gamma} \right]^{1/2} \left[ \left( \frac{D_1}{D_2} \right)^4 - 1 \right]^{-1/2}$$

from the manometer  $P_1 - P_2 = (0.2 \text{ m}) \gamma$

from the dimension given

$$\frac{D_1}{D_2} = \frac{0.1}{0.05} = 2$$

$$\left. \begin{aligned} P_1 &= \gamma h_1 \\ P_2 &= \gamma h_2 \\ P_1 - P_2 &= \gamma(h_1 - h_2) \end{aligned} \right\} \Rightarrow \left[ \left( \frac{D_1}{D_2} \right)^4 - 1 \right]^{-1/2} = \frac{1}{\sqrt{15}} = 0.2582$$

$$\therefore V_1 = \left[ 2 \left( 9.8 \frac{\text{m}}{\text{s}^2} \right) (0.2 \text{ m}) \right]^{1/2} (0.2582)$$

$$V_1 = 0.511 \text{ m/s}$$

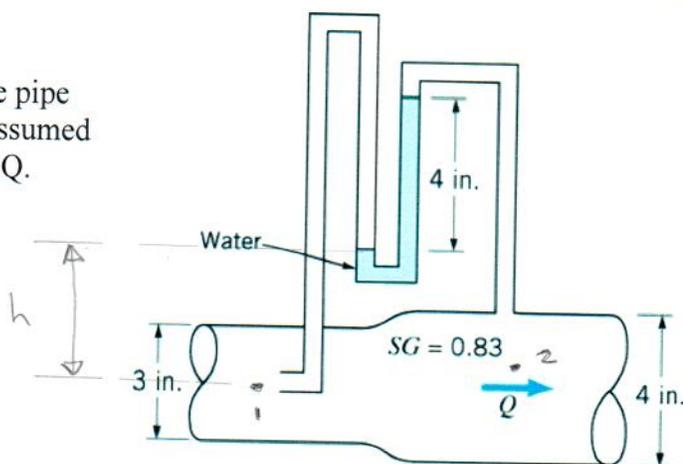
and  $Q = A_1 V_1 = \frac{\pi}{4} (0.1 \text{ m})^2 (0.511 \text{ m/s}) = 4.01 \times 10^{-3} \frac{\text{m}^3}{\text{s}}$

10 SHEETS FULLER SQUARE  
42-381 50 SHEETS FULLER SQUARE  
42-382 100 SHEETS FULLER SQUARE  
42-383 200 SHEETS FULLER SQUARE  
42-384 50 SHEETS FULLER SQUARE  
42-385 100 SHEETS FULLER SQUARE  
42-386 200 SHEETS FULLER SQUARE  
42-387 50 SHEETS FULLER SQUARE  
42-388 100 SHEETS FULLER SQUARE  
42-389 200 SHEETS FULLER SQUARE  
MADE IN U.S.A.





Oil of specific gravity 0.83 flows in the pipe section shown. If viscous effects are assumed to be negligible, estimate the flow rate  $Q$ .



First note Pts 1 and 2 on the diagram and then write Bernoulli's eqn from ① → ②

$$\frac{P_1}{\gamma_{oil}} + \frac{V_1^2}{2g} + z_1 = \frac{P_2}{\gamma_{oil}} + \frac{V_2^2}{2g} + z_2 \quad \left\{ \begin{array}{l} z_1 = z_2 \\ V_1 = 0 \text{ stagnation point} \end{array} \right.$$

$$\therefore \frac{V_2^2}{2g} = \frac{P_1 - P_2}{0.83 \gamma_w}$$

$$V_2^2 = 2.410 g \frac{P_1 - P_2}{\gamma_w}$$

Now from the manometer eqn

$$P_1 - \gamma_{oil} h - \gamma_w \left(\frac{1}{3} \text{ ft}\right) + \gamma_{oil} \left(\frac{1}{3} \text{ ft}\right) + \gamma_{oil} h = P_2$$

$$P_1 - P_2 = \gamma_w \left(\frac{1}{3} \text{ ft}\right) (1 - 0.83)$$

$$\frac{P_1 - P_2}{\gamma_w} = \left(\frac{1}{3} \text{ ft}\right) (0.17) = 0.05667 \text{ ft}$$

$$\therefore V_2 = \left[ 2.410 \left( 32.174 \frac{\text{ft}}{\text{s}^2} \right) (0.05667 \text{ ft}) \right]^{1/2}$$

$$V_2 = 2.096 \text{ ft/s}$$

and finally

$$Q = V_2 A_2 = \left( 2.096 \frac{\text{ft}}{\text{s}} \right) \frac{\pi}{4} \left( \frac{1}{3} \text{ ft} \right)^2 = 0.183 \text{ ft}^3/\text{s}$$